

# Automatic Trimming Technique for Superconducting Band-Pass Filters Using a Trimming Library

Shigetoshi OHSHIMA<sup>†a)</sup>, *Member*, Takuro KANEKO<sup>†</sup>, Jae-Hun LEE<sup>†</sup>, Maya OSAKA<sup>†</sup>, Satoshi ONO<sup>†</sup>, *Nonmembers*, and Atsushi SAITO<sup>†</sup>, *Member*

**SUMMARY** The superconducting band-pass filter has small insertion loss and excellent out-of-band rejection properties. It has been put to practical use in a number of applications. However, in order to expand its range of application, a tuning technique that can restore the filter characteristics is needed. We propose an automatic tuning system using a trimming library and checked the feasibility of the system by tuning a forward-coupled filter with three resonators. The results show that the trimming library method is an effective way of automatically improving the filter characteristics.

**key words:** HTS band-pass filter, automatic tuning, trimming library microwave device

## 1. Introduction

The superconducting band-pass filter has low loss, sharp frequency selection, and excellent noise removal characteristics [1]–[5]. A receiving band-pass filter system for the base station of wireless communications is in practical use in the United States and China [6], [7]. However, superconducting band-pass filters have gaps between their designed and measured characteristics. The existence of such gaps makes the use of such filters problematic. Gaps between design and measurement occur because of inaccurate parameters used to design the coupling coefficient between resonators, the dielectric constant, and thickness of the substrate, and resonators with different lengths [8]. In order to make such filters practical, we should restore the filter characteristics by using a trimming technique. Of the several reported trimming techniques [9]–[12], the trimming rod method is the most general [13], [14]. In this technique, a trimming rod is moved while measuring a filter characteristic. The drawback of this method is that it takes time to make an adjustment. Hence, we decided to examine the feasibility of an automatic trimming technique.

It is important to know which resonator shifts the characteristics so as to restore the filter characteristics in a short time. We previously reported on a measuring technique to determine the resonance frequency and Q value of each resonator [13], and we found that this technique could be used to restore the filter characteristics. However, it is not suitable for automatic trimming because it took a long time to measure the resonance frequency and Q value of each resonator.

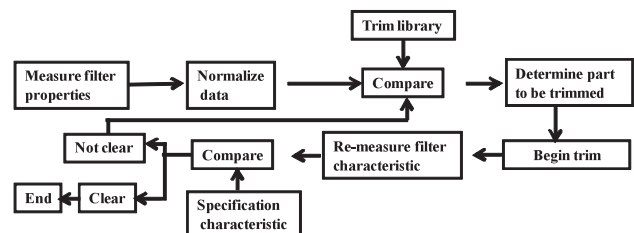
Hence, we examined the feasibility of an automatic trimming method using a trimming library and special equipment. In this paper, we describe this method briefly and discuss its effectiveness.

## 2. Automatic Trimming Process Using a Trimming Library

Figure 1 shows the flowchart of automatic trimming using a trimming library. First, the filter characteristic is measured, and then the data is normalized. The normalized technique is described in Sect. 2.1. Next, the normalized value is compared with data in the trimming library, and the trimming library data that corresponds best to the measured data is selected. The trimming library is described in Sect. 2.2. The automatic trimming system using trimming rods is described in Sect. 2.3. The trimming rod is set on the resonator, and it can be moved by a stepping motor. The process is also described in Sect. 2.3. If the restored filter characteristic after trimming meets the specifications of the filter, the trimming process stops. If the restored data do not meet the specifications, the trimming process is repeated.

### 2.1 Normalization of Measured and Library Data

To compare the characteristics of the filter against the data in the library in a short time, the data have to be normalized. Figure 2(a) shows the raw experimental data and those of an S-NAP simulation using the equivalent circuit shown in Fig. 3(b). As shown in Fig. 2(a), we found that the insertion loss and ripple have to be normalized when the library data is compared with the experimental data. We normalized the insertion loss of  $S_{21}$  and the maximum ripple to 0 and 1 dB, respectively. The reason for normalizing the maximum ripple by 1 dB is to clarify the difference between the experi-



**Fig. 1** Flowchart of automatic trimming method using a trimming library.

Manuscript received June 30, 2008.

Manuscript revised October 30, 2008.

<sup>†</sup>The authors are with the Graduate School of Science and Engineering, Yamagata University, Yonezawa-shi, 992-8510 Japan.

a) E-mail: ohshima@yz.yamagata-u.ac.jp

DOI: 10.1587/transele.E92.C.302

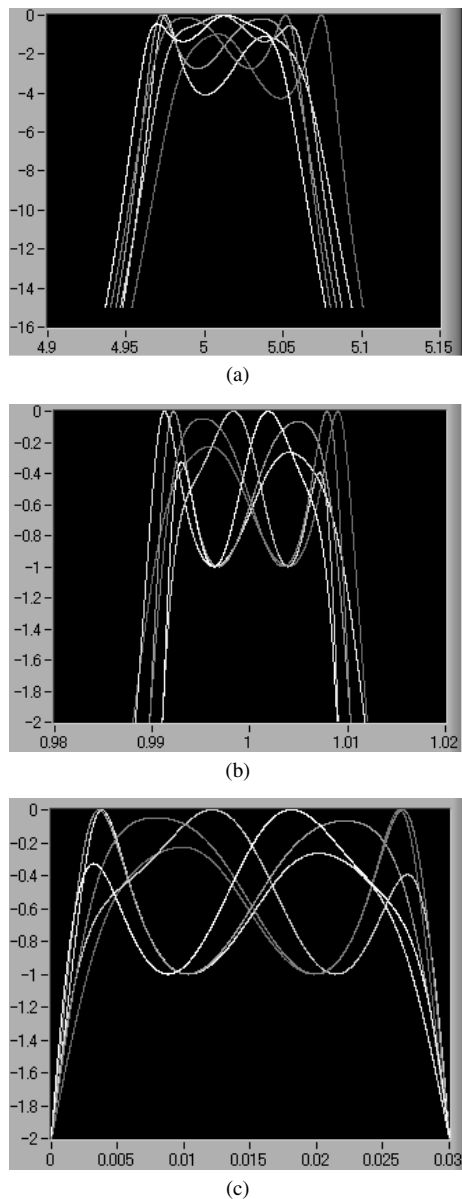


Fig. 2 Experimental and S-NAP simulation data.

mental data and library data, however the value of 1 dB is not important. The data after this processing is shown in Fig. 2(b). Next, we normalize the frequency, and since we use the Lab-View software, we have to express it numerically. The frequency range was covered by 3000 points, and it is displayed from 0 by 0.03 in figure. Moreover, the maximum value of  $S_{21}$  was assumed to be 2 dB to facilitate comparison between the library and the experimental values.

## 2.2 Trimming Library

Figures 3(a) and (b) show a three-pole forward-coupled filter configuration and its equivalent circuit. We used a conventional  $\pi$ -type equivalent circuit. First, we determined the optimum values of  $C_{in}$ ,  $C_{out}$ ,  $C_1$ ,  $C_2$ ,  $C_3$ ,  $L_1$ ,  $L_2$ , and  $L_3$  to

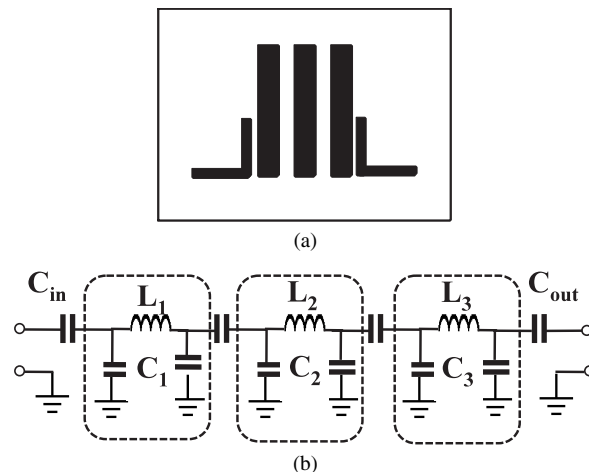


Fig. 3 Configuration of comb-type filter with three resonators and its equivalent circuit.

meet the specifications of the filter by using the S-NAP circuit simulator. Next, we calculated the filter characteristics by changing the values of  $C_1$ ,  $C_2$ , and  $C_3$ . The changes in  $C_1$ ,  $C_2$ , and  $C_3$  were assumed to be 1% or 2%. Figure 4 shows results for (a) the optimum C, (b) a 1% reduction in  $C_1$ , and (c) a 1% reduction in  $C_1$  and a 2% reduction in  $C_2$ . The filter characteristics changed greatly as C changed. We normalized the simulation data by using the same process described in 2.1. We entered these data in the trimming library. Here, L does not change. The reason is as follows. We used a sapphire trimming rod to restore the filter characteristics. Since the L element shown in the equivalent circuit in Fig. 3(b) cannot be changed, we made the trimming library in which the C element changes.

## 2.3 Trimming Procedure

We have already reported on the trimming technique for a forward-coupled filter using a sapphire rod [13]. The following is clear from our previous experiments: (1) The best sapphire rod position to change the resonance frequency of the resonator is the point that the maximum voltage is generated in the resonator. (2) The best sapphire rod position to change the coupling coefficient between resonators is the center of the gap between the resonators. The positions of the sapphire rod are shown as circles in Fig. 5(a). Figure 5(b) shows a schematic drawing of the trimming rod. The upper sapphire rod is connected to the shaft of the stepping motor, and it can be moved up and down smoothly. We developed an automatic tuning system.

Figures 6(a) and (b) show the model figure and a photograph of the system. The system consists of six modules that move the sapphire rods. The interval between the rod and the filter can be controlled by the stepping motors. The resolution of each stepping motor is  $1\ \mu\text{m}/\text{pulse}$ . The cavity for the filter is cooled by a cryocooler. The operating temperature of the filter is 70 K.

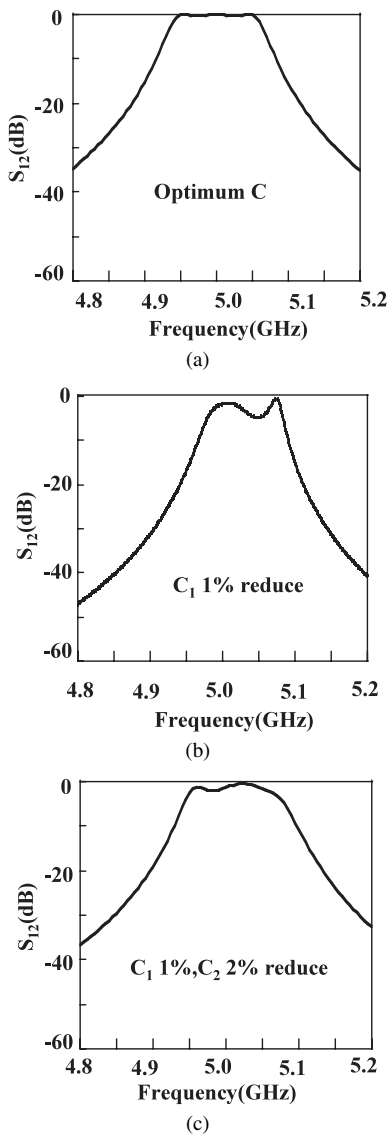


Fig. 4 Results of simulation with S-NAP circuit software: (a) optimum C, (b) 1% reduction in C<sub>1</sub>, and (c) 1% and 2% reductions in C<sub>1</sub> and C<sub>2</sub>, respectively.

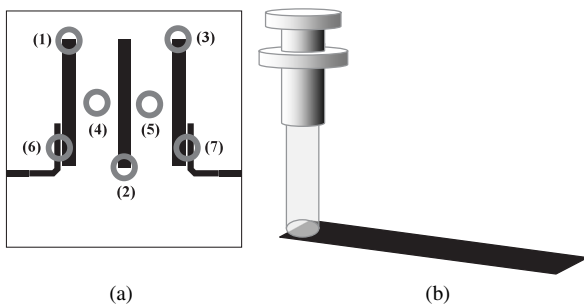


Fig. 5 Schematic drawing of filter configuration of a forward-coupled filter (a) and sapphire trimming rod (b): The circles in (a) indicate the positions of the rod trimmer.

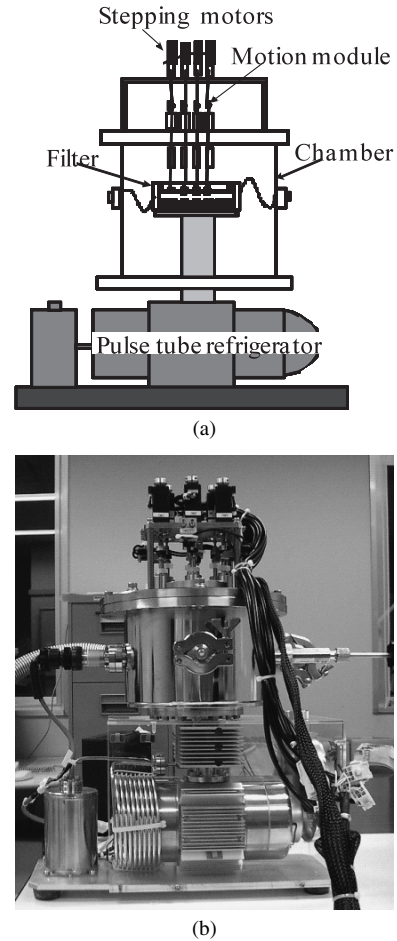


Fig. 6 Schematic drawing and picture of automatic tuning system.

### 3. Experimental Results and Discussion

Figure 7 shows the experimental and library data. The figure shows two trimming library data, one for which C<sub>1</sub> is reduced by 1% and the other for which C<sub>1</sub> and C<sub>2</sub> are reduced by 1% and 2%, respectively. We judge which library data are more suitable by referring to the following equation. The best library number was the one that gave the smallest S.

$$S = \sum_{i=1}^{3000} \sqrt{|S_i(21)_{mea} - S_i(21)_{lib}|^2}$$

where S(21) mea and S(21)lib are the measurement data and library data, respectively.

S was calculated for all data in the trimming library, and there were 12 library data for the forward-coupled filter with three resonators. From the calculation of S, we determined the best fit library, in which C<sub>1</sub> is a 1% reduction and C<sub>2</sub> is a 2% reduction.

Figure 8 shows the filter characteristics before and after trimming. The sapphire rods on resonators 1 and 2 (positions (1) and (2) in Fig. 4(a)) were shifted down to the prescribed height by using the stepping motor as shown in

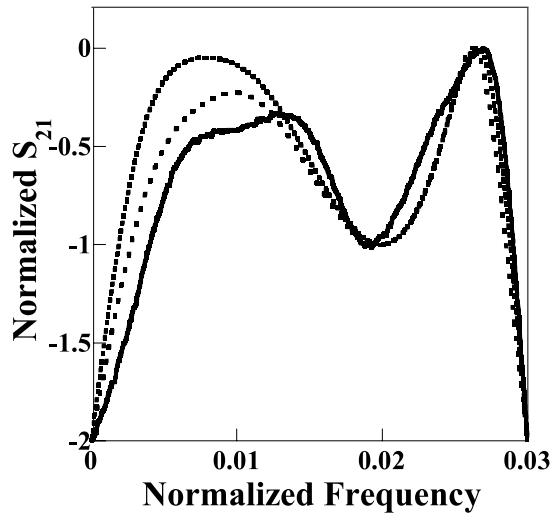


Fig. 7 Experimental and library data.

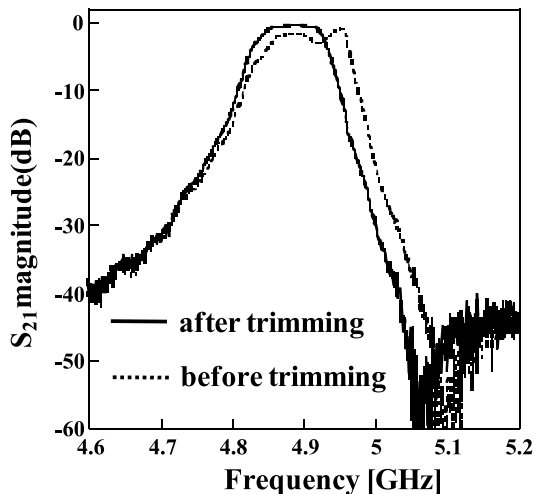


Fig. 8  $S_{21}$  filter characteristic before and after trimming.

Fig. 6(b). As shown in Fig. 8 the trimming reduced the ripple; however, the filter characteristics are not complete. We can see that there is a limit in completing the filter characteristic only by correcting C. The adjustment of the coupling strength between the feed line (positions (6) and (7) in Fig. 4(a)) and the coupling coefficient between resonators (positions (4) and (5)) is also very important for trimming. The sapphire rod can be used to make these adjustments; however, it is necessary to correct the equivalent circuit in Fig. 3(b) for that. We are now examining this adjustment.

#### 4. Conclusion

We examined the effectiveness of a trimming library technique for automatically trimming a forward-coupled filter with three resonators and obtained the following results.

(1) The sapphire rod trimmers were able to correct the ripple of the filter. The correction rods were set on the resonator edge and between the resonators.

(2) The effectiveness of the trimming library method was confirmed.

(3) The trimming rod should be set on the resonator edge and moved up and down.

(4) The heat inflow from the stepping motor shaft did not heat up the cavity. The operating temperature was kept below 70 K by using small cryocooler. (The refrigerating capacity at 70 K is 2 W.)

We need more resonators for an actual filter. Automatic tuning of such a filter is difficult with rod trimming. We are studying another trimming method for such filters and will report on it in the near future.

#### Acknowledgement

The authors would like to thank Y. Takano and M. Yokoo of Tohoku Seiki industrial Ltd. for their technical support and K. Aizawa of Yamagata University for his helpful technical support in system fabrication. This work was supported in part by the "Research and development of fundamental technologies for advanced radio frequency spectrum sharing in mobile communication systems" fund of the Ministry of Internal Affairs and Communications of Japan, and also partially supported by the Ministry of Education, Science, Sports and Culture, Grant-in-Aid for Scientific Research (C) 18560325, 2006–2008, supported by Hoso-Bunka foundation.

#### References

- [1] G. Tsuzuki, M. Suzuki, N. Sakakibara, and Y. Ueno, "Narrow-band 2 GHz superconducting filter," IEICE Trans. Electron., vol.E82-C, no.7, pp.1177–1181, July 1999.
- [2] A. Enokihara and K. Setsune, "1.5-GHz high- $T_c$  superconducting microstrip bandpass filter of miniaturized configuration," J. Supercond., vol.10, pp.49–51, Jan. 1997.
- [3] S. Ohshima, "High-temperature superconducting passive microwave devices, filters and antennas," Supercond. Sci. Technol., vol.103-108, pp.61–66, 2000.
- [4] J.-S. Hong and M.J. Lancaster, Microstrip Filters for RF/Microwave Applications, John Wiley & Sons, New York, 2001.
- [5] C. Zahopoulos, S. Sridhar, J. Bautista, G. Ortiz, and M. Lanagan, "Performance of a high  $T_c$  superconducting ultra low-loss microwave stripline filter," Appl. Phys. Lett., vol.58, pp.977–979, Sept. 1991.
- [6] R.W. Simon, "HTS technology for wireless communications," Proc. 7th International Supercond. Electronics Conf., pp.6–11, Berkeley, USA, June 1999.
- [7] Z.S. Yin, B. Wei, B.S. Cao, X.B. Guo, X.P. Zhang, W.J. He, S. He, L.M. Gao, M.H. Zhu, and B.X. Gao, "An HTS filter subsystem for 800 MHz mobile communication system," Int. J. Modern Phys., vol.19, pp.419–422, Jan. 2005.
- [8] T. Uchida, M. Suto, H. Mikami, M. Takeda, M. Kusonoki, A. Saito, M. Mukaida, and S. Ohshima, "Improvement of superconducting filter properties using sapphire rod trimming," J. Cryo. Soc. Jpn, vol.39, pp.20–26, Jan. 2004.
- [9] G.F. Dionne and D.E. Oates, "Tunability of microstrip ferrite resonator in the partially magnetized state," IEEE Trans. Magn., vol.33, no.5, pp.3421–3423, Sept. 1997.
- [10] Y. Terashima, H. Fuke, F. Aiga, M. Yamazaki, H. Kayano, and R. Kato, "2 GHz tunable superconducting band-pass filter using a piezoelectric bender," Physica C, vol.366, pp.183–189, Jan. 2002.

- [11] S. Hontsu, S. Mine, H. Nishikawa, M. Nakamor, A. Fujimaki, M. Inoue, A. Maehara, and T. Kawai, "Study of mechanical tunable superconducting microwave filter using lumped elements," *IEEE Trans. Appl. Supercond.*, vol.13, no.2, pp.720-723, June 2003.
- [12] N. Sekiya, S. Bahari, S. Kakio, Y. Nakagawa, and S. Ohshima, "Experimental study on tunable high temperature superconducting filter using novel trimming technique," *IEICE Technical Report, SCE2008-7*, April 2008.
- [13] F. Aita, N. Sekiya, S. Ono, A. Saito, S. Hirano, and S. Ohshima, "Improvement of filter properties using sapphire and nickel rod trimmers," *IEICE Trans. Electron.*, vol.E89-C, no.2, pp.119-124, Feb. 2006.
- [14] M. Osaka, S. Takeuchi, S. Ono, A. Saito, A. Akasegawa, K. Yamanaka, K. Kurihara, S. Hirano, and S. Ohshima, "Study on tuning mechanism of 5 GHz HTS filter," 20th International Symposium on Superconductivity, p.317, Tsukuba, Japan, Nov. 2007.
- [15] S. Ohshima, S. Takeuchi, M. Osaka, H. Kinouchi, S. Ono, J.-F. Lee, and A. Saito. "Examination of the resonator structure for a superconducting transmitting filter," 8th European Conference on Applied Superconductivity, p.79, Brussels, Belgium, Sept. 2007.



**Shigetoshi Ohshima** received the B.E. M.E. and D.E. degrees in Electrical Engineering of Tohoku University in 1973, 1975 and 1978, respectively. During 1978-1988, he was working on a search for new superconducting materials in Tohoku University. He moved to the Yamagata University at 1988. Since 1993, he has been Professor of Yamagata University, and in studying on the HTS microwave devices, the measurement technique of surface resistance under a high dc magnetic field, observation the vortex

of HTS materials by a Bitter method, and development of new  $J_c$  measurement system using a permanent magnet.



**Takuro Kaneko** received the B.E. degree in Electrical Engineering from Yamagata University in 2008. He was studying on the automatically tuning system of the HTS filters. He is now an employee in East Japan Railway Ltd.



**Jae-hun Lee** received the B.S., M.S. and D.S. degrees in physics of Konkoku University (Korea) in 1997, 1999, and 2006, respectively. During 1999-2006, he was working on surface resistance measurement of HTS films. Since 2006, he has been Posdoc researcher of Yamagata University, and in studying on the HTS filters.



**Maya Osaka** received the B.E. and M.E. degrees in Electrical Engineering from Yamagata University in 2006 and 2008, respectively. She was studying on the automatically tuning system of the HTS filters, and measurement of filter properties. She is now an employee in Toshiba Ltd.



**Satoshi Ono** received the B.S. and M.S. degrees in Electrical Engineering from Yamagata University in 2005 and 2007, respectively. He is student of a doctor course of Yamagata University. He is studying on the design, fabrication and examination of the HTS filters.



**Atsushi Saito** received the B.E., M.E., and D.E. degrees in Department of Electrical Engineering from Nagaoka University of Technology (NUT), Japan, in 1994, 1996, and 1999, respectively. During 1999-2001, he was a research associate in NUT. From 2001 to 2003, he was a research fellow in KARC-CRL. He is now a research associate in Faculty of Engineering, Yamagata University. His current research interests are superconducting electronics.